## APPENDIX 2

## Expressions for some common vector differential quantities in orthogonal curvilinear co-ordinate systems

 $\xi_1, \xi_2, \xi_3$  is a system of orthogonal curvilinear co-ordinates, and the unit vectors **a**, **b**, **c** are parallel to the co-ordinate lines and in the directions of increase of  $\xi_1, \xi_2, \xi_3$  respectively. The change in the position vector **x** corresponding to increments in  $\xi_1, \xi_2$ , and  $\xi_3$  can then be written as

$$\delta \mathbf{x} = h_1 \delta \xi_1 \mathbf{a} + h_2 \delta \xi_2 \mathbf{b} + h_3 \delta \xi_3 \mathbf{c}.$$

**a, b, c** and the positive scale factors  $h_1$ ,  $h_2$ ,  $h_3$  are functions of the co-ordinates. The fact that the three families of co-ordinate lines form an orthogonal system provides useful expressions for the derivatives of **a**, **b**, and **c**. We have

$$\frac{\partial \mathbf{x}}{\partial \xi_1} \cdot \frac{\partial \mathbf{x}}{\partial \xi_2} = 0,$$

with two other similar relations, and since

$$\frac{\partial}{\partial \xi_{3}} \left( \frac{\partial \mathbf{x}}{\partial \xi_{1}} \cdot \frac{\partial \mathbf{x}}{\partial \xi_{2}} \right) = \frac{\partial}{\partial \xi_{1}} \left( \frac{\partial \mathbf{x}}{\partial \xi_{3}} \right) \cdot \frac{\partial \mathbf{x}}{\partial \xi_{2}} + \frac{\partial \mathbf{x}}{\partial \xi_{1}} \cdot \frac{\partial}{\partial \xi_{2}} \left( \frac{\partial \mathbf{x}}{\partial \xi_{3}} \right)$$

$$= -2 \frac{\partial \mathbf{x}}{\partial \xi_{3}} \cdot \frac{\partial^{2} \mathbf{x}}{\partial \xi_{1}} \cdot \frac{\partial^{2} \mathbf{x}}{\partial \xi_{2}},$$
at 
$$\frac{\partial^{2} \mathbf{x}}{\partial \xi_{1}} \cdot \frac{\partial^{2} \mathbf{x}}{\partial \xi_{2}} = \frac{\partial (h_{2} \mathbf{b})}{\partial \xi_{1}} \text{ or } \frac{\partial (h_{1} \mathbf{a})}{\partial \xi_{2}},$$

is a vector normal to c. It follows that

$$\frac{\partial \mathbf{a}}{\partial \xi_2} = \frac{\mathbf{I}}{h_1} \frac{\partial h_2}{\partial \xi_1} \mathbf{b}, \quad \frac{\partial \mathbf{b}}{\partial \xi_1} = \frac{\mathbf{I}}{h_2} \frac{\partial h_1}{\partial \xi_2} \mathbf{a},$$

with four other similar relations. Then

$$\frac{\partial \mathbf{a}}{\partial \xi_1} = \frac{\partial (\mathbf{b} \times \mathbf{c})}{\partial \xi_1} = -\frac{\mathbf{i}}{h_2} \frac{\partial h_1}{\partial \xi_2} \mathbf{b} - \frac{\mathbf{i}}{h_3} \frac{\partial h_1}{\partial \xi_3} \mathbf{c},$$

with two other similar relations.

The vector gradient of a scalar function V is

grad 
$$V$$
, or  $\nabla V$ , =  $\left(\frac{\mathbf{a}}{h_1}\frac{\partial}{\partial \xi_1} + \frac{\mathbf{b}}{h_2}\frac{\partial}{\partial \xi_2} + \frac{\mathbf{c}}{h_3}\frac{\partial}{\partial \xi_3}\right)V$ .

The gradient in a direction **n** is obtained from the operator **n**.  $\nabla$ , which may act on either a scalar or a vector. To find the components of **n**.  $\nabla$ **F**, where

$$\mathbf{F} = F_1 \mathbf{a} + F_2 \mathbf{b} + F_3 \mathbf{c},$$

we must allow for the dependence of both  $F_1$ ,  $F_2$ ,  $F_3$  and the unit vectors a, b, c on position. It follows from the above relations that

$$\mathbf{n} \cdot \nabla \mathbf{F} = \mathbf{a} \left\{ \mathbf{n} \cdot \nabla F_1 + \frac{F_2}{h_1 h_2} \left( n_1 \frac{\partial h_1}{\partial \xi_2} - n_2 \frac{\partial h_2}{\partial \xi_1} \right) + \frac{F_3}{h_3 h_1} \left( n_1 \frac{\partial h_1}{\partial \xi_3} - n_3 \frac{\partial h_3}{\partial \xi_1} \right) \right\} + \mathbf{b} \left\{ \right\} + \mathbf{c} \left\{ \right\},$$

where  $n_1$ ,  $n_2$ ,  $n_3$  are the components of **n** in the directions **a**, **b**, **c**. The divergence and curl operators act only on a vector, and

$$\operatorname{div}\mathbf{F}, \quad \operatorname{or} \nabla.\mathbf{F}, \quad = \frac{\mathbf{a}}{h_1} \cdot \frac{\partial \mathbf{F}}{\partial \xi_1} + \frac{\mathbf{b}}{h_2} \cdot \frac{\partial \mathbf{F}}{\partial \xi_2} + \frac{\mathbf{c}}{h_3} \cdot \frac{\partial \mathbf{F}}{\partial \xi_3},$$

$$\operatorname{curl}\mathbf{F}, \quad \operatorname{or} \nabla \times \mathbf{F}, \quad = \frac{\mathbf{a}}{h_1} \times \frac{\partial \mathbf{F}}{\partial \xi_1} + \frac{\mathbf{b}}{h_2} \times \frac{\partial \mathbf{F}}{\partial \xi_2} + \frac{\partial \mathbf{F}}{h_3} \times \frac{\partial \mathbf{F}}{\partial \xi_3}.$$

By making use of the expressions for derivatives of a, b and c, we find

$$\nabla \cdot \mathbf{F} = \frac{1}{h_1 h_2 h_3} \left\{ \frac{\partial (h_2 h_3 F_1)}{\partial \xi_1} + \frac{\partial (h_3 h_1 F_2)}{\partial \xi_2} + \frac{\partial (h_1 h_2 F_3)}{\partial \xi_3} \right\};$$

this can also be regarded as the result of applying the 'divergence theorem' to the small parallelepiped whose edges are displacements along co-ordinate lines corresponding to the increments  $\delta \xi_1$ ,  $\delta \xi_2$ ,  $\delta \xi_3$ . Likewise we find

$$\nabla \times \mathbf{F} = \frac{\mathbf{a}}{h_2 h_3} \left\{ \frac{\partial (h_3 F_3)}{\partial \xi_2} - \frac{\partial (h_2 F_2)}{\partial \xi_3} \right\} + \frac{\mathbf{b}}{h_3 h_1} \left\{ \frac{\partial (h_1 F_1)}{\partial \xi_3} - \frac{\partial (h_3 F_3)}{\partial \xi_1} \right\} + \frac{\mathbf{c}}{h_1 h_2} \left\{ \frac{\partial (h_2 F_2)}{\partial \xi_1} - \frac{\partial (h_1 F_1)}{\partial \xi_2} \right\} + \frac{\mathbf{c}}{h_1 h_2} \left\{ \frac{\partial (h_2 F_2)}{\partial \xi_1} - \frac{\partial (h_1 F_1)}{\partial \xi_2} \right\}$$
or 
$$\frac{\mathbf{I}}{h_1 h_2 h_3} \begin{vmatrix} \partial & \partial & \partial \\ \partial \xi_1 & \partial \xi_2 & \partial \xi_3 \\ \partial \xi_2 & \partial \xi_3 \end{vmatrix},$$

which can also be regarded as following from the application of Stokes's theorem in turn to three orthogonal faces of the same parallelepiped.

The divergence of the gradient gives the *Laplacian* operator, which may act on either a scalar or a vector.

$$\begin{split} \nabla.\nabla V, \quad \text{or } \nabla^2 V, \quad &= \frac{1}{h_1 h_2 h_3} \left\{ \frac{\partial}{\partial \xi_1} \left( \frac{h_2 h_3}{h_1} \frac{\partial V}{\partial \xi_1} \right) \right. \\ &+ \frac{\partial}{\partial \xi_2} \left( \frac{h_3 h_1}{h_2} \frac{\partial V}{\partial \xi_2} \right) + \frac{\partial}{\partial \xi_3} \left( \frac{h_1 h_2}{h_3} \frac{\partial V}{\partial \xi_3} \right) \right\}. \end{split}$$

The components of  $\nabla^2 \mathbf{F}$  may be calculated by replacing V in this formula by  $\mathbf{F}_1 = F_1 \mathbf{a} + F_2 \mathbf{b} + F_3 \mathbf{c}$ , and using the expressions for derivatives of  $\mathbf{a}$ ,  $\mathbf{b}$  and  $\mathbf{c}$ , but the result is too complicated to be useful. It is usually more convenient,

when finding the components of  $\nabla^2 \mathbf{F}$  in a particular co-ordinate system, to  $\nabla^2 \mathbf{F} = \nabla(\nabla \cdot \mathbf{F}) - \nabla \times (\nabla \times \mathbf{F})$ 

and the above expressions for grad, div and curl.

the fixed direction m is system. The gradient, in the direction n, of the component of velocity u in terms of velocity components and derivatives relative to the curvilinear Consider now the components of the rate-of-strain tensor expressed in

$$\mathbf{n} \cdot \nabla (\mathbf{m} \cdot \mathbf{u}), = \mathbf{m} \cdot (\mathbf{n} \cdot \nabla \mathbf{u}).$$

to Cartesian axes locally parallel to a, b and c (to which the suffixes 1, 2, 3 gradients for which m and n are orthogonal. We see then, from the above obtained by putting  $\mathbf{m} = \mathbf{n}$ , and the non-diagonal elements involve velocity formula for  ${f n}$  .  $abla {f F}$ , that the components of the rate-of-strain tensor relative Diagonal elements of the rate-of-strain tensor represent rates of extension,

$$\begin{aligned} e_{11} &= \mathbf{a} \cdot (\mathbf{a} \cdot \nabla \mathbf{u}) = \frac{1}{h_1} \frac{\partial u_1}{\partial \xi_1} + \frac{u_2}{h_1 h_2} \frac{\partial h_1}{\partial \xi_2} + \frac{u_3}{h_3 h_1} \frac{\partial h_1}{\partial \xi_3}, \\ e_{23} &= \frac{1}{2} \mathbf{b} \cdot (\mathbf{c} \cdot \nabla \mathbf{u}) + \frac{1}{2} \mathbf{c} \cdot (\mathbf{b} \cdot \nabla \mathbf{u}) = \frac{h_3}{2h_2} \frac{\partial}{\partial \xi_2} \left(\frac{u_2}{h_3}\right) + \frac{h_2}{2h_3} \frac{\partial}{\partial \xi_3} \left(\frac{u_2}{h_2}\right), \end{aligned}$$

strain, using the relation (for an incompressible fluid) components of the stress tensor  $\sigma_{ij}$  can be obtained from those of rate of with four other expressions obtained by cyclic interchange of suffixes. The

$$\sigma_{ij} = -p\,\delta_{ij} + 2\mu e_{ij}.$$

The components of all terms in the equation of motion of a fluid in the directions a, b, c may now be found by simple substitution in the appropriate expressions above. The components of the term  ${f u}$  .  $abla {f u}$  in the acceleration are obtained from the expression for **n**.  $\nabla \mathbf{F}$ .

Applications to some particular co-ordinate systems are as follows

## Spherical polar co-ordinates

To the co-ordinates  $\xi_1 = r$ ,  $\xi_2 = \theta$ ,  $\xi_3 = \phi$  (where  $\phi$  is the azimuthal angle about the axis  $\theta = 0$ ) there correspond the scale factors

Then 
$$\begin{aligned} h_1 &= \mathbf{1}, & h_2 &= r, & h_3 &= r\sin\theta. \\ \frac{\partial \mathbf{a}}{\partial r} &= \mathbf{o}, & \frac{\partial \mathbf{a}}{\partial \theta} &= \mathbf{b}, & \frac{\partial \mathbf{a}}{\partial \phi} &= \sin\theta \, \mathbf{c}, \\ \frac{\partial \mathbf{b}}{\partial r} &= \mathbf{o}, & \frac{\partial \mathbf{b}}{\partial \theta} &= -\mathbf{a}, & \frac{\partial \mathbf{b}}{\partial \phi} &= \cos\theta \, \mathbf{c}, \\ \frac{\partial \mathbf{c}}{\partial r} &= \mathbf{o}, & \frac{\partial \mathbf{c}}{\partial \theta} &= -\sin\theta \, \mathbf{a} - \cos\theta \, \mathbf{b}. \end{aligned}$$

$$\nabla V &= \mathbf{a} \frac{\partial V}{\partial r} + \frac{\mathbf{b}}{r} \frac{\partial V}{\partial \theta} + \frac{\mathbf{c}}{r\sin\theta} \frac{\partial V}{\partial \phi},$$

Common vector differential quantities

$$\mathbf{n}.\nabla \mathbf{F} = \mathbf{a} \left( \mathbf{n}.\nabla F_{r} - \frac{n_{\phi}F_{\phi}}{r} - \frac{n_{\phi}F_{\phi}}{r} \right) + \mathbf{b} \left( \mathbf{n}.\nabla F_{\phi} - \frac{n_{\phi}F_{\phi}}{r} \cot \theta + \frac{n_{\phi}F_{\gamma}}{r} \right) + \mathbf{c} \left( \mathbf{n}.\nabla F_{\phi} + \frac{n_{\phi}F_{\gamma}}{r} \cot \theta + \frac{n_{\phi}F_{\gamma}}{r} \right) + \mathbf{c} \left( \mathbf{n}.\nabla F_{\phi} + \frac{n_{\phi}F_{\gamma}}{r} \cot \theta + \frac{n_{\phi}F_{\gamma}}{r} \right) + \mathbf{c} \left( \mathbf{n}.\nabla F_{\phi} + \frac{n_{\phi}F_{\gamma}}{r} \cot \theta + \frac{n_{\phi}F_{\gamma}}{r} \cot \theta \right),$$

$$\nabla \cdot \mathbf{F} = \frac{\mathbf{i}}{r\sin \theta} \left\{ \frac{\partial (r^{2}F_{\gamma})}{\partial r} + \frac{\mathbf{i}}{r\sin \theta} \frac{\partial (\sin \theta F_{\phi})}{\partial \theta} + \frac{\mathbf{i}}{r\sin \theta} \frac{\partial F_{\phi}}{\partial \phi} + \frac{\partial F_{\gamma}}{\partial r} \right\} + \frac{\mathbf{c}}{r} \left\{ \frac{\partial (rF_{\phi})}{\partial r} - \frac{\partial F_{\gamma}}{\partial \theta} \right\},$$

$$\nabla^{2}F = \frac{\mathbf{i}}{r^{2}} \frac{\partial (F_{\phi}\sin \theta)}{\partial r} + \frac{\mathbf{i}}{r^{2}\sin \theta} \frac{\partial F_{\phi}}{\partial \theta} + \frac{\mathbf{i}}{r^{2}\sin^{2}\theta} \frac{\partial F_{\phi}}{\partial \phi} + \frac{\partial F_{\gamma}}{\partial \theta} \right\},$$

$$\nabla^{2}F = \mathbf{a} \left\{ \nabla^{2}F_{\gamma} - \frac{2F_{\gamma}}{r^{2}} - \frac{2}{r^{2}\sin \theta} \frac{\partial (F_{\phi}\sin \theta)}{\partial \theta} - \frac{2}{r^{2}\sin^{2}\theta} \frac{\partial F_{\phi}}{\partial \phi} \right\}$$

$$+ \mathbf{b} \left\{ \nabla^{2}F_{\phi} + \frac{2}{r^{2}\sin \theta} \frac{\partial F_{\gamma}}{\partial \theta} - \frac{2}{r^{2}\sin^{2}\theta} \frac{\partial F_{\phi}}{\partial \phi} - \frac{F_{\phi}}{r^{2}\sin^{2}\theta} \frac{\partial F_{\phi}}{\partial \phi} \right\}.$$

Rate-of-strain tensor:

$$\begin{split} e_{rr} &= \frac{\partial u_r}{\partial r}, \quad e_{\theta\theta} = \frac{1}{r} \frac{\partial u_\theta}{\partial \theta} + \frac{u_r}{r}, \quad e_{\phi\phi} = \frac{1}{r \sin \theta} \frac{\partial u_\phi}{\partial \phi} + \frac{u_r}{r} + \frac{u_\theta \cot \theta}{r}, \\ e_{\theta\phi} &= \frac{\sin \theta}{2r} \frac{\partial}{\partial \theta} \left( \frac{u_\phi}{\sin \theta} \right) + \frac{1}{2r \sin \theta} \frac{\partial u_\theta}{\partial \phi}, \quad e_{\phi r} = \frac{1}{2r \sin \theta} \frac{\partial u_r}{\partial \phi} + \frac{r}{2} \frac{\partial}{\partial r} \left( \frac{u_\phi}{r} \right), \\ e_{r\theta} &= \frac{r}{2} \frac{\partial}{\partial r} \left( \frac{u_\theta}{r} \right) + \frac{1}{2r} \frac{\partial u_r}{\partial \theta}. \end{split}$$

Equation of motion for an incompressible fluid, with no body force:

$$\frac{\partial u_r}{\partial t} + \mathbf{u} \cdot \nabla u_r - \frac{u_0^2}{r} - \frac{u_0^2}{r} = -\frac{\mathbf{i}}{\rho} \frac{\partial p}{\partial r} + \nu \left\{ \nabla^2 u_r - \frac{2u_r}{r^2} - \frac{2}{r^2 \sin \theta} \frac{\partial (u_\theta \sin \theta)}{\partial \theta} - \frac{2}{r^2 \sin \theta} \frac{\partial u_\phi}{\partial \phi} \right\},$$

$$\frac{\partial u_\theta}{\partial t} + \mathbf{u} \cdot \nabla u_\theta + \frac{u_r u_\theta}{r} - \frac{u_\theta^2 \cot \theta}{r} = -\frac{\mathbf{i}}{\rho r} \frac{\partial p}{\partial \theta} + \nu \left\{ \nabla^2 u_\theta + \frac{2}{r^2} \frac{\partial u_r}{\partial \theta} - \frac{u_\theta}{r^2 \sin^2 \theta} - \frac{2 \cos \theta}{r^2 \sin^2 \theta} \frac{\partial u_\phi}{\partial \phi} \right\},$$

$$\frac{\partial u_\phi}{\partial t} + \mathbf{u} \cdot \nabla u_\phi + \frac{u_\phi u_r}{r} + \frac{u_\theta u_\phi \cot \theta}{r} = -\frac{\mathbf{i}}{\rho r \sin \theta} \frac{\partial p}{\partial \phi} + \frac{2 \cos \theta}{r^2 \sin^2 \theta} \frac{\partial u_\phi}{\partial \phi} - \frac{u_\phi}{r^2 \sin^2 \theta} \right\},$$

$$\frac{\partial u_\phi}{\partial t} + \mathbf{u} \cdot \nabla u_\phi + \frac{u_\phi u_r}{r} + \frac{u_\theta u_\phi \cot \theta}{r} = -\frac{\mathbf{i}}{\rho r \sin \theta} \frac{\partial p}{\partial \phi} + \frac{2 \cos \theta}{r^2 \sin^2 \theta} \frac{\partial u_\phi}{\partial \phi} - \frac{u_\phi}{r^2 \sin^2 \theta} \right\},$$

of the x-co-ordinate line, but are written out here in view of the frequency of

Cylindrical co-ordinates

To the co-ordinates  $\xi_1 = x$ ,  $\xi_2 = \sigma$ ,  $\xi_3 = \phi$  (where  $\phi$  is the azimuthal angle about the axis  $\sigma = 0$ ) there correspond the scale factors

$$h_1 = I, \quad h_2 = I, \quad h_3 = \sigma.$$

$$\frac{\partial \mathbf{a}}{\partial \phi} = \mathbf{o}, \quad \frac{\partial \mathbf{b}}{\partial \phi} = \mathbf{c}, \quad \frac{\partial \mathbf{c}}{\partial \phi} = -\mathbf{b},$$

and a, b, c are independent of x and  $\sigma$ .

$$\begin{split} \nabla V &= \mathbf{a} \frac{\partial V}{\partial x} + \mathbf{b} \frac{\partial V}{\partial \sigma} + \frac{\mathbf{c}}{\sigma} \frac{\partial V}{\partial \phi}, \\ \mathbf{n} \cdot \nabla \mathbf{F} &= \mathbf{a} (\mathbf{n} \cdot \nabla F_x) + \mathbf{b} \left( \mathbf{n} \cdot \nabla F_\sigma - \frac{n_\phi F_\phi}{\sigma} \right) + \mathbf{c} \left( \mathbf{n} \cdot \nabla F_\phi + \frac{n_\phi F_\sigma}{\sigma} \right), \\ \nabla \cdot \mathbf{F} &= \frac{\partial F_x}{\partial x} + \frac{\mathbf{i}}{\sigma} \frac{\partial (\sigma F_\sigma)}{\partial \sigma} + \frac{\mathbf{i}}{\sigma} \frac{\partial F_\phi}{\partial \phi}, \end{split}$$

$$\nabla \cdot \mathbf{F} = \frac{\partial F_x}{\partial x} + \frac{\mathbf{i}}{\sigma} \frac{\partial (\sigma F_\phi)}{\partial \sigma} + \frac{\mathbf{i}}{\sigma} \frac{\partial F_\phi}{\partial \phi},$$

$$\nabla \times \mathbf{F} = \mathbf{a} \left\{ \frac{\mathbf{i}}{\sigma} \frac{\partial (\sigma F_\phi)}{\partial \sigma} - \frac{\mathbf{i}}{\sigma} \frac{\partial F_\sigma}{\partial \phi} \right\} + \mathbf{b} \left( \frac{\mathbf{i}}{\sigma} \frac{\partial F_x}{\partial \phi} - \frac{\partial F_\phi}{\partial x} \right) + \mathbf{c} \left( \frac{\partial F_\sigma}{\partial x} - \frac{\partial F_x}{\partial \sigma} \right)$$

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\mathbf{i}}{\sigma} \frac{\partial}{\partial \sigma} \left( \sigma \frac{\partial V}{\partial \sigma} \right) + \frac{\mathbf{i}}{\sigma^2} \frac{\partial^2 V}{\partial \phi^2},$$

$$\nabla^2 \mathbf{F} = \mathbf{a} (\nabla^2 F_x) + \mathbf{b} \left( \nabla^2 F_\sigma - \frac{F_\sigma}{\sigma^2} - \frac{2}{\sigma^2} \frac{\partial F_\phi}{\partial \phi} \right) + \mathbf{c} \left( \nabla^2 F_\phi + \frac{2}{\sigma^2} \frac{\partial F_\sigma}{\partial \phi} - \frac{F_\phi}{\sigma^2} \right).$$

Rate-of-strain tensor:

$$e_{xx} = \frac{\partial u_x}{\partial x}, \quad e_{\sigma\sigma} = \frac{\partial u_\sigma}{\partial \sigma}, \quad e_{\phi\phi} = \frac{1}{\sigma} \frac{\partial u_\phi}{\partial \phi} + \frac{u_\sigma}{\sigma},$$

$$e_{\sigma\phi} = \frac{\sigma}{2} \frac{\partial}{\partial \sigma} \left( \frac{u_{\phi}}{\sigma} \right) + \frac{1}{2\sigma} \frac{\partial u_{\sigma}}{\partial \phi}, \quad e_{\phi x} = \frac{1}{2\sigma} \frac{\partial u_{x}}{\partial \phi} + \frac{1}{2} \frac{\partial u_{\phi}}{\partial x}, \quad e_{x\sigma} = \frac{1}{2} \frac{\partial u_{\sigma}}{\partial x} + \frac{1}{2} \frac{\partial u_{x}}{\partial \sigma}$$

Equation of motion for an incompressible fluid, with no body force:

$$\begin{split} \frac{\partial u_x}{\partial t} + \mathbf{u} \cdot \nabla u_x &= -\frac{\mathbf{i}}{\rho} \frac{\partial \underline{p}}{\partial x} + \nu \nabla^2 u_x, \\ \frac{\partial u_\sigma}{\partial t} + \mathbf{u} \cdot \nabla u_\sigma - \frac{u_\phi^2}{\sigma} &= -\frac{\mathbf{i}}{\rho} \frac{\partial \underline{p}}{\partial \sigma} + \nu \left( \nabla^2 u_\sigma - \frac{u_\sigma}{\sigma^2} - \frac{2}{\sigma^2} \frac{\partial u_\phi}{\partial \phi} \right), \\ \frac{\partial u_\phi}{\partial t} + \mathbf{u} \cdot \nabla u_\phi + \frac{u_\sigma u_\phi}{\sigma} &= -\frac{\mathbf{i}}{\rho \sigma} \frac{\partial \underline{p}}{\partial \phi} + \nu \left( \nabla^2 u_\phi + \frac{2}{\sigma^2} \frac{\partial u_\sigma}{\partial \phi} - \frac{u_\phi}{\sigma^2} \right). \end{split}$$

Polar co-ordinates in two dimensions

The relevant formulae can be obtained from those for the above cylindrical co-ordinates by suppressing all components and derivatives in the direction

their use. The co-ordinates are  $\xi_1 = r$ ,  $\xi_2 = \theta$ , and  $h_1 = r$ ,  $h_2 = r$ ,

$$\xi_1 = r$$
,  $\xi_2 = \theta$ , and  $h_1 = 1$ ,  $h_2 = r$ ,
$$\frac{\partial \mathbf{a}}{\partial r} = 0$$
,  $\frac{\partial \mathbf{a}}{\partial \theta} = \mathbf{b}$ ,  $\frac{\partial \mathbf{b}}{\partial r} = 0$ ,  $\frac{\partial \mathbf{b}}{\partial \theta} = -\mathbf{a}$ .
$$\nabla V = \mathbf{a} \frac{\partial V}{\partial r} + \frac{\mathbf{b}}{2r} \frac{\partial V}{\partial r}$$

$$\begin{split} \mathbf{n} \cdot \nabla \mathbf{F} &= \mathbf{a} \left( \mathbf{n} \cdot \nabla F_r - \frac{n_\theta F_\theta}{r} \right) + \mathbf{b} \left( \mathbf{n} \cdot \nabla F_\theta + \frac{n_\theta F_r}{r} \right), \\ \nabla \cdot \mathbf{F} &= \frac{\mathbf{i}}{r} \frac{\partial (rF_r)}{\partial r} + \frac{\mathbf{i}}{r} \frac{\partial F_\theta}{\partial \theta}, \\ \nabla \times \mathbf{F} &= \left\{ \frac{\mathbf{i}}{r} \frac{\partial (rF_\theta)}{\partial r} - \frac{\mathbf{i}}{r} \frac{\partial F_r}{\partial \theta} \right\} \mathbf{a} \times \mathbf{b}, \\ \nabla^2 V &= \frac{\mathbf{i}}{r} \frac{\partial}{\partial r} \left( r \frac{\partial V}{\partial r} \right) + \frac{\mathbf{i}}{r^2} \frac{\partial^2 V}{\partial \theta^2}, \\ \nabla^2 F &= \mathbf{a} \left( \nabla^2 F_r - \frac{F_r}{r^2} - \frac{2}{r^2} \frac{\partial F_\theta}{\partial \theta} \right) + \mathbf{b} \left( \nabla^2 F_\theta + \frac{2}{r^2} \frac{\partial F_r}{\partial \theta} - \frac{F_\theta}{r^2} \right). \end{split}$$

Rate-of-strain tensor:

$$e_{rr} = \frac{\partial u_r}{\partial r}, \quad e_{\theta\theta} = \frac{1}{r} \frac{\partial u_{\theta}}{\partial \theta} + \frac{u_r}{r}, \quad e_{r\theta} = \frac{r}{2} \frac{\partial}{\partial r} \left(\frac{u_{\theta}}{r}\right) + \frac{1}{2r} \frac{\partial u_r}{\partial \theta}.$$

Equation of motion for an incompressible fluid, with no body force:

$$\begin{split} \frac{\partial u_r}{\partial t} + \left(u_r \frac{\partial}{\partial r} + \frac{u_\theta}{r} \frac{\partial}{\partial \theta}\right) u_r - \frac{u_\theta^2}{r} &= -\frac{\mathbf{I}}{\rho} \frac{\partial p}{\partial r} + \nu \left(\nabla^2 u_r - \frac{u_r}{r^2} - \frac{\mathbf{Z}}{r^2} \frac{\partial u_\theta}{\partial \theta}\right), \\ \frac{\partial u_\theta}{\partial t} + \left(u_r \frac{\partial}{\partial r} + \frac{u_\theta}{r} \frac{\partial}{\partial \theta}\right) u_\theta + \frac{u_r u_\theta}{r} &= -\frac{\mathbf{I}}{\rho r} \frac{\partial p}{\partial \theta} + \nu \left(\nabla^2 u_\theta + \frac{\mathbf{Z}}{r^2} \frac{\partial u_r}{\partial \theta} - \frac{u_\theta}{r^2}\right). \end{split}$$