

Ship Hydrodynamics

MidTerm - I

Oct. 23, 2014

- 1) If Froude's law of similarity is valid, then Moment coefficients should be equal: $C_{M_m} = C_{M_s}$, that is: $\frac{M_m}{\frac{\rho_m}{2} S_m V_m^2 L_m} = \frac{M_s}{\frac{\rho_s}{2} S_s V_s^2 L_s}$ 5

$$\therefore \frac{M_s}{M_m} = \left(\frac{\rho_s}{\rho_m}\right) \left(\frac{S_s}{S_m}\right) \left(\frac{V_s}{V_m}\right)^2 \left(\frac{L_s}{L_m}\right) = \frac{\rho_s}{\rho_m} (\lambda^2) (\sqrt{\lambda})^2 (\lambda) = \frac{\rho_s}{\rho_m} \lambda^4$$
 10

$$\therefore M_s = M_m \left(\frac{\rho_s}{\rho_m}\right) \lambda^4 = 39.5 \left(\frac{1025}{1000}\right) (30)^4 = \underline{32794.9 \text{ kN}\cdot\text{m}}$$
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- 2) If the two ships are in the same medium

$$\alpha^3 = \frac{V_B}{V_A} = \frac{\rho_A^{1/2} 12000}{\rho_B^{1/2} 8000} = 1.5 \Rightarrow \alpha = 1.145$$

$$V_A = 12 \text{ kn} = 6.173 \text{ m/s} \Rightarrow V_B = \sqrt{\alpha} V_A = 6.605 \text{ m/s} = 12.84 \text{ kn}$$
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Since $\frac{C_F}{C_R} = 1.2$ in both ships; $C_F = 1.2 C_R$, or;

$$C_T = 0.6 C_T + C_R$$

$$\text{Ship A: } (C_T \rho^{1/2} S V^2)_A = 147.5 \text{ kN @ } 12 \text{ kn} \Rightarrow C_{T_A} = 2.85 \times 10^{-3}$$

$$C_{T_A} = 0.6 C_{T_A} + C_{R_A} \Rightarrow C_{R_A} = 0.4 C_{T_A} = 1.140 \times 10^{-3}$$
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Ship B: $C_{T_B} = 0.6 C_{T_B} + C_{R_B}$. Since at the corresponding speeds;

$$C_{R_A} = C_{R_B}; \quad C_{T_B} = \frac{C_{R_B}}{0.4} = 2.85 \times 10^{-3}$$
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$$\therefore R_{R_B} = C_{R_B} \frac{\rho}{2} S_B V_B^2 = 1.140 \times 10^{-3} \left(\frac{1025}{2}\right) (\alpha^2 S_A) (\alpha V_A^2) = 88.56 \text{ kN}$$
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$$\text{and } R_{T_B} = \frac{R_{R_B}}{0.4} = 221.4 \text{ kN}$$
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$$\text{Finally; } P_{E_B} = V_B \cdot R_{T_B} = 1462 \text{ kW @ } 12.84 \text{ kn.}$$
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$$3) Re_s = \left(\frac{VL}{\nu}\right)_s = \frac{\sqrt{\alpha} V_m L_s}{\nu_s} = \frac{(10.29)(154.6)}{1.18732 \times 10^{-6}} = 1.339 \times 10^9$$

$$C_{F_s} = \frac{0.075}{[\log(Re_s) - 2]^2} = \frac{0.075}{[\log(1.339 \times 10^9) - 2]^2} = 1.4766 \times 10^{-3}$$
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$$C_A = [105 \left(\frac{k_s}{L_s}\right)^{1/3} - 0.64] \times 10^{-3} = [105 \left(\frac{150 \times 10^{-6}}{154.6}\right)^{1/3} - 0.64] \times 10^{-3} = 0.3995 \times 10^{-3}$$

Model scale wave resistance; $C_w = C_{T_m} - (1+k) C_{F_m}$

$$L_m = \frac{L_s}{\alpha} = \frac{154.6}{26} = 5.95 \text{ m}, \quad S_m = \frac{S_s}{\alpha^2} = \frac{5670}{(26)^2} = 8.388 \text{ m}^2$$

$$Re_m = \frac{V_m L_m}{\nu_m} = \frac{(2.018)(5.95)}{1.02333 \times 10^{-6}} = 1.173 \times 10^7$$

$$\therefore C_{Fm} = \frac{0.075}{[\log(1.173 \times 10^7) - 2]^2} = 2.919 \times 10^{-3}$$

$$C_{Tm} = \frac{R_{Tm}}{\rho/2 S_m V_m^2} = \frac{75.9}{\frac{1000}{2} \times 8.388 \times (2.018)^2} = 4.444 \times 10^{-3}$$

$$\therefore C_w = C_{Tm} - (1+k)C_{Fm} = [4.444 - (1.280)(2.919)] \times 10^{-3} = 0.708 \times 10^{-3} \quad \underline{5}$$

Total ship resistance:

$$C_{Ts} = (1+k)C_{Fs} + C_w + C_A = [(1.280)(1.4766) + 0.708 + 0.3995] \times 10^{-3} \\ = 2.998 \times 10^{-3} \quad \underline{5}$$

$$\text{Finally: } R_{Ts} = \left(\frac{\rho}{2} S V^2\right)_s C_{Ts} = \frac{1025}{2} \times 5670 \times (10.29)^2 \times 2.998 \times 10^{-3} \\ = 922.4 \text{ kN} \quad \underline{5}$$

HP 0.746 kW

$$P_{Es} = R_{Ts} \cdot V_s = 922.4 \times 10.29 = 9491.5 \text{ kW} = 12723 \text{ HP} \quad \underline{5}$$

4. a) Two methods employing series (family) of ships can be cited: "ITU Balika Gemisi Serisi" and UBC trawler series. Ortmeressen's statistical/empirical method may also be used.
- b) No. Because thin-ship theory does not account ^{for} the viscosity.
- c) Adverse pressure gradient means positive gradient in pressure ¹⁰ which causes separation by retarding the flow.